



# COMPARITIVE ANALYSIS OF INTERLINE POWER FLOW CONTROLLER WITH PI &FUZZY LOGIC CONTROLLER

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## ABSTRACT

Cost of the transmission lines plays a vital role in the network company. Because of the various practical constraints, the transmission lines are often only utilized for a fraction of its individual limits. To improve the economical aspects one possibility would be to add to the value of transmission lines by transport large amount of energy through those lines. One of the solutions to this problem will be a FACTS technology. An Interline Power Flow Controller (IPFC) is a converter-based FACTS controller for series compensation with capability of controlling power flow among multi-lines within the same corridor of the transmission line. In this paper, it is proposed to develop the Interline power flow controller using Pi controller and Fuzzy Logic Controller. The basic characteristics of IPFC are to be analysed on two similarly dimensioned parallel transmission lines. The model has to be simulated with Matlab simulink program to demonstrate system behavior of interline power flow controller. Numerical results are to be demonstrated on the IEEE 30 Bus system with the Interline power flow controller model. It has to be validating that there is a possibility of regulating active power flow, reactive power flow and minimizing the power losses simultaneously with proposed IPFC parameter.

**Keywords:** Flexible AC Transmission System (FACTS), Voltage Source Converter (VSC), Interline Power Flow Controller (IPFC), PI Controller, Fuzzy Controller.

## I. INTRODUCTION

In general the FACTS controller can be divided into two groups: converter based FACTS controller and Non-converter based FACTS controller. Non-converter based FACTS controller include Static Var compensator (SVC) and Thyristor-controlled series capacitor (TCSC) have the advantage of generating or absorbing reactive power without the use of ac capacitors and reactors. Converter based FACTS controller include STATCOM, SSSC, UPFC and IPFC which has the capability of individually control the active and reactive power flow on the transmission line. The basic concept of FACTS controller are clearly explained in the book, 'understanding FACTS concepts and Technology of Flexible The detailed explanation about series connected FACTS controller



such as Static Synchronous Series compensator (SSSC) and Interline power flow controller given in [2, 3]. Both SSSC and IPFC have the capable of operating in capacitive/ inductive mode. The Unified Power Flow Controller (UPFC) is an combination of two FACTS device such as STATCOM and SSSC linked together with the common DC link, were as the IPFC consist of two are more than two SSSC linked together with the common DC link. Each SSSC provide the reactive power compensation to the individual line were it connected and also it has the capable of transmitting the real power from underutilized line to the overloaded line these concepts was explained in [4]. The paper [5] a simple mathematical model of IPFC was proposed for the optimal control of power flow on the transmission lines. Mathematical models of generalized unified power flow controller (GUPFC) and IPFC and their implementation in Newton power flow are demonstrate in [6].

In the year 2002 a basic characteristic of Voltage Source Converter based Interline Power Flow Controller was discussed in paper [7] by the author Jianhong chen etal. Along with two basic control scheme, namely (i) Special Control Scheme and (ii) General control Scheme. The Special control scheme is designed for the power flow control of a transmission system with two identical parallel lines while the general control scheme can be used to solve the power flow control problem in a multi-line transmission system. Both special and general control schemes are based on the decoupled PI controller. A current source converter topology based inter line power flow controller was proposed in paper [8], along with decoupled stat-feedback control for the injected voltage with a separated dc current controller. Here the dynamic model of the system is derived and divided into a liner part and a nonlinear part. The linear part is controlled in an inner loop by a decoupled state-feedback controller. The nonlinear part is controlled in an outer loop by a PI controller which regulates the dc side current.

In paper [9] the regulation model of an Interline Power Flow Controller and its control strategies at rated capacity was discussed. Rated capacity operation is important in determining the maximum power transfer capability under voltage stability conditions. A model decomposition approach is proposed to select the best damping control input signals. The proposed technology was demonstrated on a 20-bus testsystem. The dispatch result shows that the IPFC improve the power transfer in the system. The author Sasan Salem proposed a two 3-level neutral point clamped voltage source converter for interline power flow controller in paper [10]. In this proposal interline power flow controller was designed to compensate the impedances of two similarly dimensioned parallel transmission lines. The behavior of the system under various transient and load changes at the receiving-end of the transmission system was presented. The interline power flow controller has the capability in compensating both resistance and reactance of the transmission line, and maintaining the dc-link voltage constant. The dc link voltage is balanced by using a balancing circuit based on zero sequence current.

In this paper a detailed switching level simulation model of IPFC was developed on the Matlab Simulink environment. Here the IPFC was developed to compensate the impedance of the transmission line.

An in-direct controller Strategy was developed to controller the power flow on the transmission line i.e. the power flows on the transmission line was controlled by varying the active impedance of the transmission line. The controller is also otherwise called as reactance controller as in [10]. The performance on the IPFC on the parallel transmission line was demonstrated. IEEE 30 Bus system was modeled in the Simulink and it performance was investigated without IPFC,IPFC with PI,Fuzzy logic controllers. Three different case studies were carry out on the practical 30 Bus system to study the dynamic behavior of the IPFC. Power flow analysis at

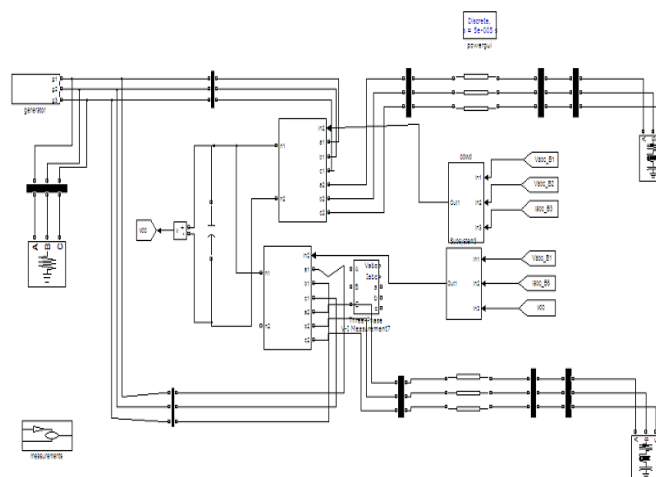
base load, 10% increasing in load condition and under fault condition were carryout without IPFC,IPFC with PI, Fuzzy logic controllers.

## II. PROBLEM FORMULATION

The losses in the Transmission Line and demand on the power system increased gradually. The increasing in Losses and demand is fulfilled either by increasing the generation or by improving the existing system. FACTS technology is essential to alleviate some of the problem but not all of these difficulties. Converter based FACTS controller have the capability to control both active and reactive power flow on the transmission line. The line current and injected voltage the effective reactance of the transmission line is varied. SSSC is used to control the power flow in single transmission line whereas the IPFC is used to control the powerflow power flow on the multi transmission line.

## III. INTERLINE POWER FLOW CONTROLLER

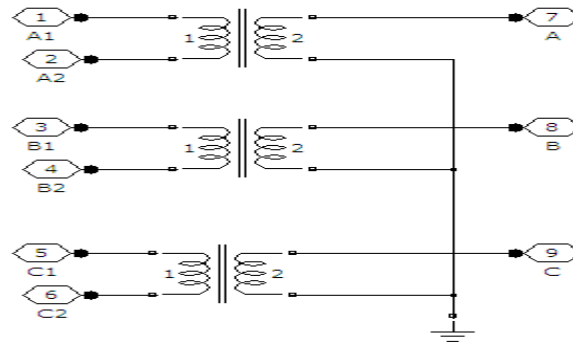
IPFC consist of a number of DC to AC inverters, each inverter providing reactive power compensation to the different line. IPFC can also view as a combination of number of SSSC linked together at their DC terminals. A detailed simulink model of IPFC is shown in the Fig. 1. With this configuration any of the inverter can be controlled to supply the real power to the common DC link from its own transmission line. Thus the overall surplus power can be made to utilize from the lightly loaded line to overloaded line. For analysis purpose let as consider the IPFC consist of two Voltage source converters among which converter 1 will act as the master which control the power flow on the line one independent of the line 2. Converter 2 on the line 2 is meant for maintaining the DC link voltage irrespective of variation in supply. The simulink model consists of Generator, IPFC, Parallel transmission lines and two loads. The generator is modeled using three phase voltage source followed by impedance. The values of generator parameters are given in the Appendix I.



**Fig.1.Simulink model of IPFC**

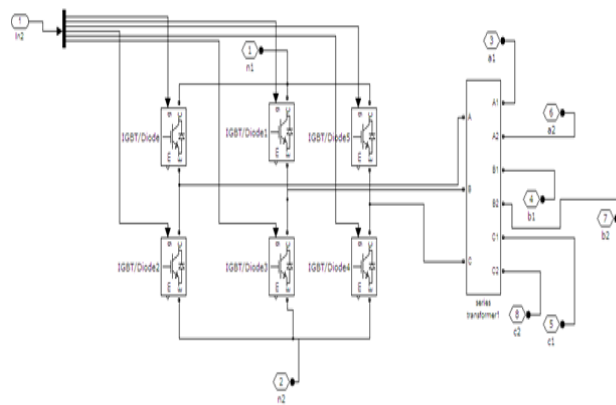
Voltage source converters are connected in series with the transmission line through the series transformer which is shown in Fig. 2 and Fig. 3. The rating of the series transformer and the value of the DC link capacitance are given in the Appendix II. The transmission lines are constructed using the distributed parameter block available in the simulink environment. The value of the transmission line parameter and loads on the line 1 and line 2 are

given in Appendix III.



**Fig.2.Series Transformer along With VSC**

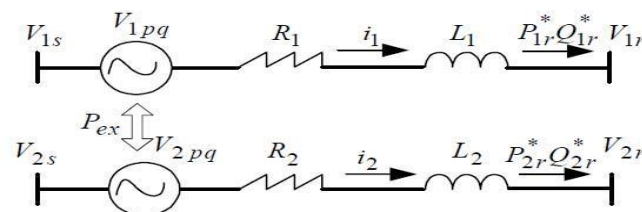
In case of UPFC the active power demand of the series converter was supplied by the shunt device. However in IPFC the active power demand of one series inverter is compensated by another series inverter. The power exchange between two inverters depending on the current flows through the transmission lines.



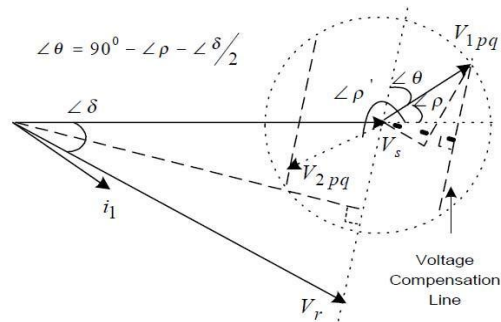
**Fig.3.Simulink Model of VSC along With Series Transformer**

**IV. CONTROL STRATEGY**

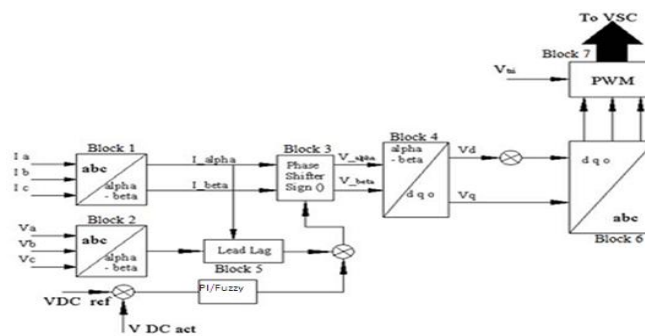
In this paper, the IPFC is designed to regulating the impedance of the transmission line. The primary IPFC consist of two converter system. A converter1 system, that is capable of regulating impedances of Line 1. A converter2 system regulates dc-link voltage of the VSC at a desired level.



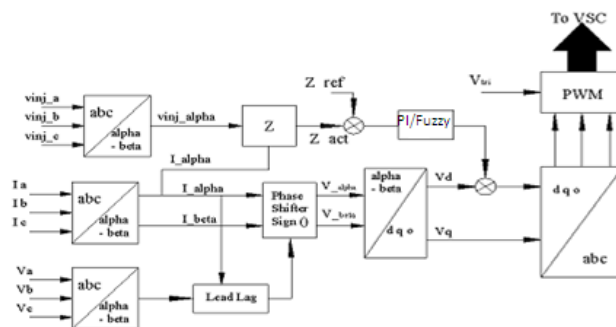
**Fig.4.Equivalent Circuit of IPFC**



**Fig.5. Vector Diagram**



**Fig.6. Control Circuit of Slave converter**



**Fig.7. Control Circuit of Master Converter**

Fig. 6 shows the block diagram for the slave system. Block 1 is used to transform the three phase voltage injected by the VSC ( $V_{inj\_a}$ ,  $V_{inj\_b}$ , and  $V_{inj\_c}$ ) in to the two phases as the equation (1). Block 2 is used to transform the three phase line currents ( $I_a$ ,  $I_b$  and  $I_c$ ) in to two phase  $I_\alpha$  &  $I_\beta$  similar to equation (1).

$$\begin{bmatrix} V_{inj-\alpha} \\ V_{inj-\beta} \\ V_{inj-0} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{pmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & \frac{\sqrt{3}}{2} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \frac{-1}{\sqrt{2}} \end{pmatrix} \begin{bmatrix} V_{inj-a} \\ V_{inj-b} \\ V_{inj-c} \end{bmatrix} \quad (1)$$

Block 5 (Lead/ Lag Block) receives the reference signal of the line voltage  $V_\alpha$  and from block 3 and the reference signal of the line current  $I_\alpha$  from block 2 and computes the  $90^\circ$  phase shift and its sign. This information is summed with the output angle from the DC voltage controller. Block 3 receives the  $I_\alpha$  and  $I_\beta$  reference signals from block 2. These signals are modulated by the sum of the signals from the DC voltage controller and Lead/ Lag blocks to generate the modified reference signals  $V_\alpha'$  and  $V_\beta'$ . Block 4 is the  $\alpha - \beta - 0$  to  $d - q - 0$  transformation block used to convert the two phase reference components in stationary frame  $V_\alpha'$  and  $V_\beta'$  to two phase reference component in synchronously rotating frame  $V_d'$  and  $V_q'$  as per the equation (5). These signals are then fed to PWM trigger unit to generate the pulse.

$$\begin{bmatrix} S_d \\ S_q \\ S_0 \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{pmatrix} \cos wt & \sin wt & 0 \\ -\sin wt & \cos wt & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{bmatrix} S_a \\ S_b \\ S_c \end{bmatrix} \quad (2)$$

Fig.7 shows the overall control structure of the master IPFC system. This block diagram is similar to the block diagram of the slave IPFC system and has many of the same blocks except for two major differences: (a) the dc voltage controller and (b) Impedance controller. Since the dc link voltage is controlled by the slave system, the dc voltage controller no longer needed. In order to control the impedance of the transmission line 1 impedance controller is added in addition to the slave controller. To regulate the injected impedance, an impedance Controller is used. The injected impedance  $Z_{inj-1}$  is compared to a reference  $Z_{ref}$  and error is fed to a PI controller. The resultant is added to the d- component of the desired reference waveform  $V_d'$ . Block 6 receives the modified d- and q- components  $V_d'$  and  $V_q'$  and transform them to three phase coordinated as per the equation 6, these signals are used as the reference signals  $V_a^*$ ,  $V_b^*$  and  $V_c^*$  of PWM controller and Block Provides Firing pulses for SVC switched.

### 4.1. PI controller

In this paper PI controller is used to improve the power transfer capability in multi Transmission Lines. Discrete PI controller block was used in simulation of IPFC by keeping  $K_p=18.3$ ,  $K_i=4.3$

### 4.2. Fuzzy Logic Controller

In this paper fuzzy controller also used to improve the power transfer capability in multi Transmission Lines. then compare the performance of IPFC to IEEE 30 Bus system without IPFC, IPFC with PI and Fuzzy logic Controller. Fuzzy rules are framed with the combination of error and change in error. they are in Table 1.

**Table 1 Fuzzy rules**

Error/Error rate	NB	NM	NS	Z	PS	PM	PB
NB	NB	NB	NB	NM	NM	NS	Z
NM	NB	NB	NM	NM	NS	Z	PS
NS	NB	NM	NM	NS	Z	PS	PM
Z	NM	NM	NS	Z	PS	PM	PM
PS	NM	NS	Z	PS	PM	PM	PB
PM	NS	Z	PS	PM	PM	PB	PB
PB	Z	PS	PM	PM	PB	PB	PB

## V. SYSTEM DESCRIPTION

It consists of six generating units, 41-transmissionlines, two VAR injecting sources, and four tap changing transformers. The base real power demand of the system is281.43MW and the base reactive power demand of the system is 134.3KVAR. The single line diagram of the IEEE 30 bus system is given in Appendix IV and its simulation diagram is shown inFig8.The line data and the bus data are given in reference[11]. To study the dynamic behavior of the IPFC on the IEEE 30 bus system power flow analysis were carry out. The voltage profile, real power flow and reactive power flow at various buses are measured which was discussed in simulation results.

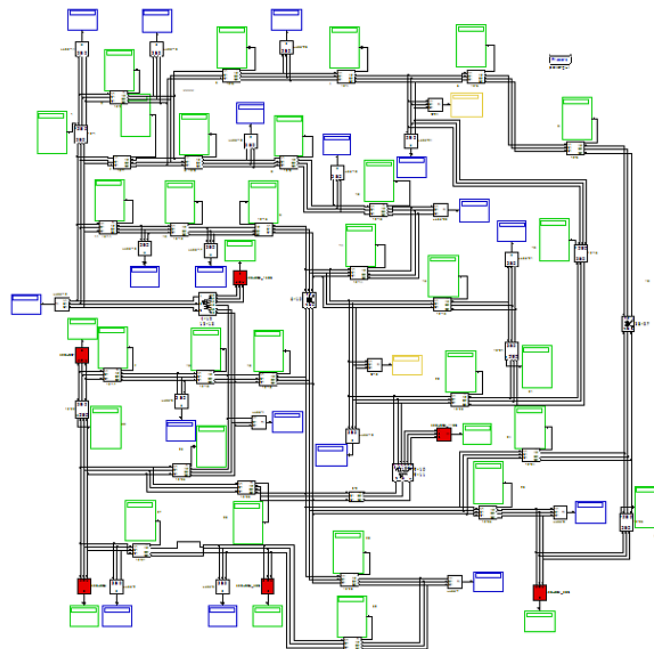
### 5.1. IEEE-30 Bus Systems

It consists of six generating units, 41 transmission lines, and the base real power demand of the system is 281.4MW and reactive power demand of the system is 134.3 MVar.The Interline power flow controller is connected between the line 1-2 and line 5-13. Three case studies are carried out to analysis the effect of IPFC on the practical utility system.

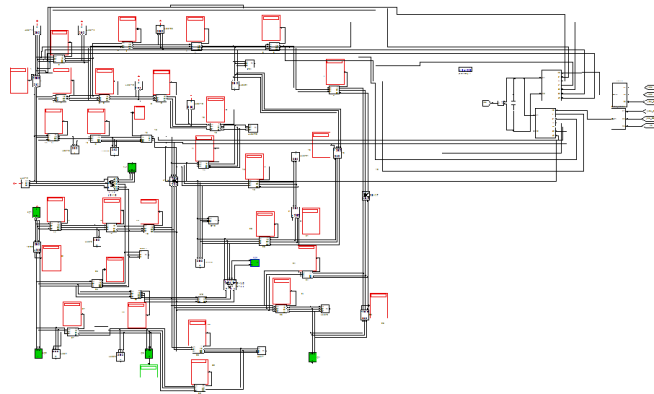
Case 1: Base load condition

Case 2: 10% increasing in load at all the Buses

Case 3: Fault condition (three phase fault in the line 6-10)



**Fig.8 Simulation diagram of IEEE 30 bus system without IPFC**

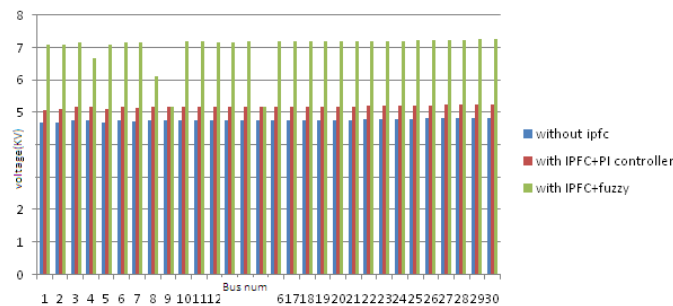


**Fig.9 Simulation diagram of IEEE 30 bus system with IPFC**

## VI. SIMULATION RESULTS AND DISCUSSION

### Case 1: Base load Condition

Load flow analysis on the 30 Bus systems is carryout with and without Interline power flow controller at base load condition. The Base active and reactive power demand of the system are 281.4MW and 134.3MVar respectively. Voltage profile and real and reactive power at various buses are measured which is give in the table 2. From the illustration, it is inferred that before placing the interline power flow controller the average voltage profile at all the buses was found to be 0.94pu, after placing the IPFC between the line 1-2 and line 5-13 the average voltage profile at all the buses improved to 1.02pu. The real and reactive power delivered to all the loads also increased. The comparison of various parameter bus voltages, real and reactive powers at various buses are given in Fig.10 to12



**Fig.10 Voltage at various buses under base load condition**

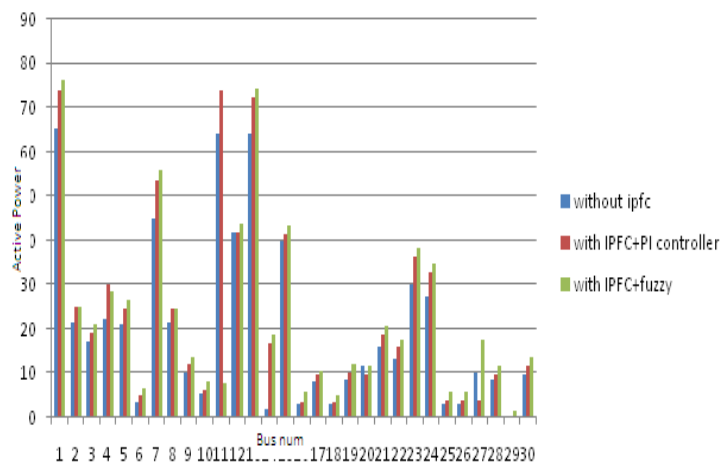
**Table 2 Result under base load condition**

Base Load Condition									
Bus No.	Without IPFC			With IPFC+PI			With IPFC+Fuzzy		
	VB	P	Q	VB	P	Q	VB	P	Q
1	4.7	65.4	-54.3	5.1	74.2	-67.1	7.08	76	-68.6
2	4.7	21.7	-18.2	5.1	25	-20.5	7.1	25	-16.3
3	4.8	17.3	-17.6	5.2	19.3	-21.4	7.17	21	-23.4

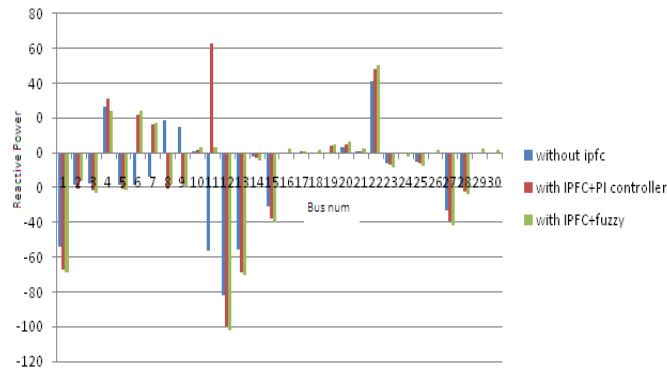




4	4.8	22.2	26.69	5.2	30.1	31.2	6.67	29	24.52
5	4.7	21.3	-18.2	5.1	24.6	-20.5	7.11	27	-21.5
6	4.8	3.67	-18.8	5.2	5.03	22.2	7.18	6.5	24.2
7	4.7	45.1	-14.1	5.2	53.8	16.41	7.15	56	17.51
8	4.8	21.4	18.6	5.2	24.6	-21	6.12	25	-18.2
9	4.8	10.2	14.77	5.2	12.1	-17.4	5.2	14	-19.4
10	4.8	5.3	1.18	5.2	6.26	1.4	7.2	8.3	2.896
11	4.8	64.2	-56.1	5.2	74.1	63.22	7.2	7.8	3.396
12	4.8	42	-82.2	5.2	42	-100	7.18	44	-102
13	4.8	64.3	-55.9	5.2	72.2	-69.1	7.18	74	-70.6
14	4.8	2.15	-2.44	5.2	16.7	-3.01	7.19	19	-4.51
15	4.8	40	-30.9	5.2	41.6	-37.9	5.19	44	-39.9
16	4.8	3.2	0.16	5.2	3.72	0.19	7.19	5.7	2.244
17	4.8	8.24	0.53	5.2	9.7	0.63	7.19	11	0.626
18	4.8	2.96	0.08	5.2	3.45	0.1	7.19	5	1.597
19	4.8	8.69	0.31	5.2	10.3	3.67	7.19	12	5.168
20	4.8	11.6	3.29	5.2	9.67	4.72	7.19	12	6.32
21	4.8	16	1.02	5.2	18.9	1.21	7.2	21	2.709
22	4.8	13.4	41.16	5.2	16.2	48.47	7.21	18	50.47
23	4.8	30.3	-5.78	5.2	36.5	-7.06	7.21	39	-8.56
24	4.8	27.4	-0.39	5.2	33	-0.71	7.22	35	-2.21
25	4.8	3.25	-5.35	5.2	3.8	-6.32	7.23	5.8	-7.82
26	4.8	3.25	0.21	5.2	3.83	0.25	7.23	5.8	1.751
27	4.8	10.3	-33.4	5.2	4.11	-39.4	7.24	18	-41.4
28	4.8	8.51	-19.2	5.2	9.75	-22.5	7.25	12	-24
29	4.8	0	0.01	5.3	0	0.1	7.26	1.5	2.099
30	4.8	9.94	0.13	5.3	11.7	0.21	7.26	14	1.71



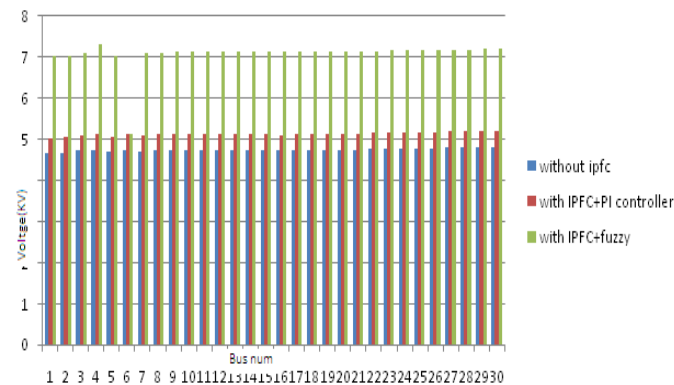
**Fig.11 Voltage at various buses under base load condition**



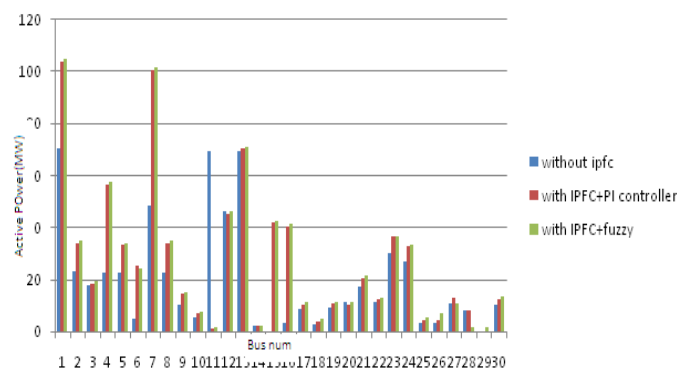
**Fig.12 Voltage at various buses under base load condition**

### Case 2: 10% increasing in load at all the Buses

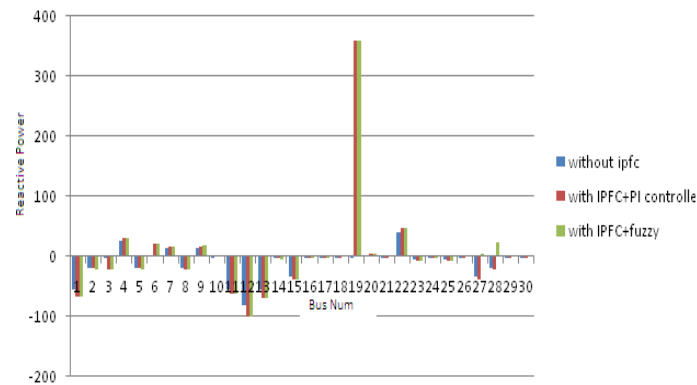
In this case the active power demand at all the buses is increased by 10%, the real power demand of the system is keeping at 309.54MW. The reactive power demand remains same as the base value 134.3MVar and load flow analysis is carryout with and without IPFC. From the load flow result it is inferred that due to increasing in load demand the voltage profile at all the buses reduced further when compared to the base load condition. After placing the IPFC between the lines 1-2 to line 5-13, the system will able to maintain the voltage profile within the allowable limit. Load flow result under 10% increases in load condition is given in the Table 3 and the comparisons of various parameters are given in Fig. 13 to Fig. 15.



**Fig.13 Voltage at all buses under 10% increase in load condition**



**Fig.14 Active Power at all buses under 10% increase in load condition**



**Fig.15 Reactive Power at all buses under 10% increase in load condition**

**Table 3 Results under 10% increase in load condition**

10% increase in Load Condition									
Bus No.	Without IPFC			With IPFC+PI			Without IPFC+Fuzzy		
	VB	P	Q	VB	P	Q	VB	P	Q
1	4.7	70.7	-53.8	5	104	-66.38	7.03	105	-66.9
2	4.7	23.4	-18	5.1	33.9	-19.78	7.05	34.9	-20.8
3	4.7	18	-1.73	5.1	18.2	-21.06	7.11	19.2	-21.6
4	4.7	22.8	25.93	5.1	56.7	30.44	7.31	57.7	30.94
5	4.7	23	-18	5.1	33.2	-19.82	7.05	33.7	-20.8
6	4.7	5.29	1.85	5.1	25.3	22.01	5.13	24.3	21.01
7	4.7	48.8	13.91	5.1	101	15.8	7.1	102	16.3
8	4.7	23.1	-18.4	5.1	33.8	-20.24	7.12	34.8	-20.7
9	4.8	10.6	14.57	5.1	14.7	17.05	7.14	15.2	18.05
10	4.8	5.76	1.17	5.1	6.74	1.37	7.14	7.74	1.866
11	4.8	69.6	-55.3	5.1	1.01	-61.01	7.14	1.51	-62
12	4.7	46.8	-81.1	5.1	45.1	-98.88	7.12	46.1	-99.9
13	4.7	69.7	-55.1	5.1	70.5	-68.35	7.12	71	-69.4
14	4.7	2.49	-2.41	5.1	1.9	-2.97	7.13	2.4	-3.97
15	4.7	0.42	-33	5.1	42.1	-37.31	7.13	42.6	-38.3
16	4.8	3.47	0.16	5.1	40.6	0.19	7.13	41.6	-2
17	4.8	8.93	0.52	5.1	10.4	0.61	7.13	11.1	-1.9
18	4.8	3.17	0.08	5.1	3.71	0.1	7.14	4.71	1.595
19	4.8	9.43	0.31	5.1	11	358.9	7.14	11.5	359.9
20	4.8	11.8	3.24	5.1	10.2	4.84	7.14	11.2	5.81
21	4.8	17.4	1.01	5.1	20.3	1.18	7.14	21.3	1.683
22	4.8	11.5	40.63	5.2	12.5	47.4	7.15	13	48.4
23	4.8	30.3	-5.69	5.2	36.4	-6.94	7.16	36.9	-7.94
24	4.8	27.1	-0.38	5.2	32.6	-0.73	7.16	33.1	-2.23
25	4.8	3.53	-5.28	5.2	4.13	-6.18	7.17	5.13	-6.68
26	4.8	3.52	0.21	5.2	4.24	0.25	7.18	7.12	1.746

27	4.8	11.1	-32.9	5.2	13	-38.53	7.19	11	3.79
28	4.8	8.66	-18.9	5.2	8.24	-21.92	7.19	1.64	22.92
29	4.8	0	0.01	5.2	0	0.1	7.2	1.5	2.097
30	4.8	10.8	0.18	5.2	12.3	0.21	7.2	13.3	1.606

### Case 3: Fault condition

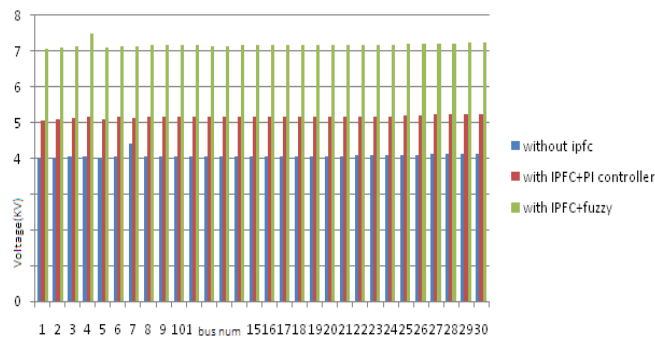
To analysis the effectiveness of IPFC on the power flow management under fault condition, in this case a three phase short circuit fault is created in the line 6-10 with fault resistance 500 ohm. Due to occurrence of the three phase fault the average voltage profile at all the buses are reduced from 0.94pu to 0.8pu. Were as after placing the IPFC in the system, it will able to maintain the voltage profile within the allowable limit and it will able to deliver the required power to the load. Load flow result under fault condition is given in the Table 4 and the comparisons of various parameters are given in Fig. 16 to Fig. 18.

**Table 4 Results under Fault condition**

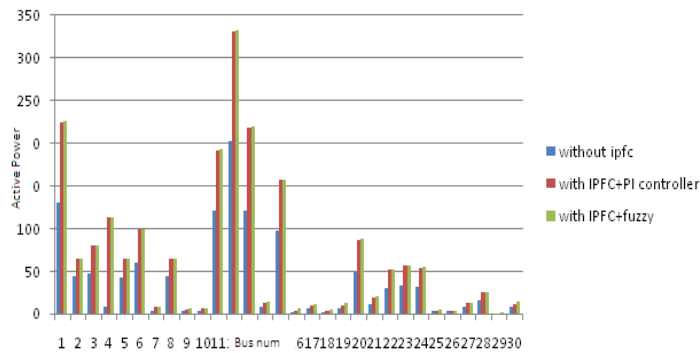
fault Condition									
Bus No.	Without IPFC			With IPFC+PI			Without IPFC+Fuzzy		
	VB	P	Q	VB	P	Q	VB	P	Q
1	4	130.3	-39.3	5.1	225	-73.3	7.06	227	75.33
2	4	43.33	-13.2	5.1	64.1	-17.8	7.09	65.1	-18.8
3	4.1	47.79	-12.6	5.1	79.7	-22.2	7.14	80.7	-22.7
4	4.1	7.74	-19.8	5.2	113	-32.2	7.51	114	-33
5	4	43	-13.2	5.1	63.8	-18	7.09	64.3	-18.8
6	4.1	59.97	-12.6	5.2	98.2	-20.6	7.15	98.9	-21.1
7	4.4	3.7	10.22	5.1	7.13	15.5	7.13	7.63	16.54
8	4.1	43.2	-13.5	5.2	64.1	-18.3	7.17	64.6	-17.3
9	4.1	2.91	10.81	5.2	4.97	17.4	7.17	5.97	17.95
10	4.1	3.88	0.86	5.2	6.19	1.38	7.17	6.97	19.45
11	4.1	121	-40.7	5.2	192	-55.3	7.16	193	-56.8
12	4.1	202.3	-60.4	5.2	332	-108	7.15	333	-109
13	4.1	120.9	-40.5	5.2	218	-75.7	7.15	219	-76.2
14	4.1	8.32	-1.95	5.2	12.4	-3.58	7.16	13.4	-4.18
15	4.1	97.31	-22.7	5.2	157	-409	7.16	157	-408
16	4.1	2.32	0.12	5.2	3.73	0.19	7.16	5.73	1.692
17	4.1	5.98	0.38	5.2	9.6	0.62	7.16	11.2	2.119
18	4.1	2.12	0.06	5.2	3.4	0.1	7.17	4.62	1.596
19	4	6.3	0.23	5.2	10.1	362.	7.17	12.1	3.644
20	4.1	49.07	-2.95	5.2	86	8.09	7.17	88	9.59
21	4.1	11.63	0.74	5.2	18.7	1.2	7.17	20.7	2.696

22	4.1	30.33	-29.9	5.2	51.2	47.9	7.18	52	48.06
23	4.1	32.81	-3.92	5.2	56.1	-7.06	7.18	56.3	-8.7
24	4.1	30.66	-0.01	5.2	52.6	-0.78	7.18	54.6	-2.27
25	4.1	2.36	-3.88	5.2	3.8	-6.26	7.2	4.45	-6.52
26	4.1	2.36	0.15	5.2	3.79	2.49	7.21	2.79	3.993
27	4.1	7.44	24.2	5.2	12	-39	7.22	13	30.99
28	4.1	15.99	14.06	5.2	24.9	-22.2	7.22	25.1	25.1
29	4.1	0	0.06	5.2	0	0.1	7.23	2	1.599
30	4.1	7.21	0.13	5.2	11.6	0.28	7.23	13.6	2.281

**Table 4 Results under Fault condition**



**Fig.16 Voltage at all buses under Fault condition**



**Fig.17 Active Power at all buses under Fault condition**



**Fig.18 Reactive Power at all buses under Fault condition**



## VII. CONCLUSION AND FUTURE SCOPE

In this project, the detailed model of Inter line Power Flow Controller (IPFC) with PI controller and Fuzzy controller was implemented to the IEEE 30 bus system. IEEE 30 bus system analyzed with the IPFC for three Different cases i.e, base load condition, 10%increase in Load condition and fault condition.From the power flow result we conclude that the Interline power flow controller increase the power transfer capability in the IEEE 30 bus system with PI controller and Fuzzy controller. Fuzzy controller gives better results compared to PI controller.

In this paper only IEEE 30 Bus System with PI controller and Fuzzy controller was simulated, In future change the Bus System and Controller by ANN technology or any other advanced evolutionary algorithms and compare the performance of IPFC with any other FACTS devices.

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## Appendix I

RMS value of Line voltage : 500 KV

Source frequency : 50Hz

Phase angle : 9.2°

Source resistance : 1.4706Ω

Source inductance : 39mH

## Appendix II

Rating of the series transformer : 100MVA

RMS value of the phase voltage : 50/50KV

Winding resistance : 0.05pu

Winding inductance : 0.05pu

Magnetizing resistance & inductance: 500Ω each

DC link capacitance : 2500μf

## Appendix III

### Transmission line parameter

No of phase : 3

Length of transmission line : 75Km

Resistance :  $R_1=0.0255\Omega$ ,  $R_0=0.3864\Omega$

Inductance :  $X_1=0.9337mH$ ,  $X_0=4.1264mH$

Capacitance :  $C_1=12.74nf$ ,  $C_0=7.751nf$

### Rating of the loads

Active power : 4000MW

Reactive power : 3000MVAR (inductive)

Load voltage : 500KV

## Appendix IV

### Single line diagram of 30 bus system

